

Artificial Neural Network Controlled DSTATCOM for Power Quality Improvement

S. Sherin Jasper

M.E. Department of Power electronics and drives, Sri Shakthi Institute of engineering and technology,
Coimbatore, Tamil Nadu. India

Abstract: The paper intends to develop the artificial neural network control algorithm for the control of DSTATCOM for the improvement of power quality. The presence of nonlinear loads makes the voltage to be deviated and current to be distorted from its sinusoidal waveform quality. Thus harmonics elimination, load balancing and voltage regulation is the heavy task that has to be accomplished to maintain the quality of the power. The performance of any device depends on the control algorithm used for the reference current estimation and gating pulse generation scheme. Thus the artificial neural network based Back Propagation (BP) algorithm has been proposed to generate the triggering pulses for the three phase H bridge inverter (DSTATCOM). The fundamental weighted value of active and reactive power components of load currents which are required for the estimation of reference source current is calculated by using BP-based control algorithm. Based on the difference of the target voltage and the generated voltage, the triggering pulse for the inverter is obtained by the BP algorithm. Then the voltage is injected at the point of common coupling to compensate the reactive power. Thus by regulating the voltage and compensation of reactive power, the power quality can be improved. The simulation modelling of the Back propagation algorithm controlled DSTATCOM and the PWM controlled DSTATCOM and the comparative analysis of the algorithms is presented in this paper.

Index Term: DSTATCOM, Artificial Neural Network, Back propagation (BP) control algorithm, Reference current Estimation, Power quality.

I. MOTIVATION

Power quality in distribution systems affects all the electrical and electronics equipment that are connected. This measures the deviation in the measurement of frequency, current and Voltage of the system. The use of power converters in power supplies, adjustable speed drives, is continuously increasing in recent years. This equipment draws harmonics currents from AC mains and increases the supply demands. The classification of loads includes linear (lagging power factor loads), nonlinear (current or voltage source type of harmonic generating loads), unbalanced and mixed types of loads. The power quality problems associated with these loads include, load unbalancing, harmonics, high reactive power burden, voltage variation.

The power quality problems are compensated in a distribution system by the Custom Power devices. These custom power devices are classified as the DSTATCOM (Distribution Static Compensator), DVR (Dynamic Voltage Restorer) and UPQC (Unified Power Quality Conditioner). The power quality at the Point of common coupling is governed by standards such as IECSC77A , IEEE-519-1992, IEEE-1531-2003 and IEC- 61000, etc.

The block diagram of the proposed system consists of the three phase supply supplying the nonlinear load, DSTATCOM block, interfacing inductor, and the DSTATCOM controller. The DSTATCOM controller used in this project is the Back Propagation method, which is the neural network controlled algorithm.

The effectiveness of DSTATCOM depends upon the control algorithm used for generating the switching signals for the voltage source converter and value of interfacing inductors. Many control algorithms are reported in the literature based on the instantaneous reactive power theory, deadbeat or predictive control instantaneous symmetrical component theory nonlinear control technique , modified power balance theory, enhanced phase locked loop technique, Adaline control technique, synchronous reference frame control technique, ANN and fuzzy based controller, SVM based controller, correlation and cross-correlation coefficients based control algorithm for the control of DSTATCOM. In this Paper, the designed system will be applied to detect transient voltage in electrical power systems. The problem of power quality is detected by artificial neural network based BP algorithm. The performance of the designed system will be tested through a simulation platform designed in MATLAB/Simulink.

II. BLOCK DIAGRAM OF ANN CONTROLLED DSTATCOM

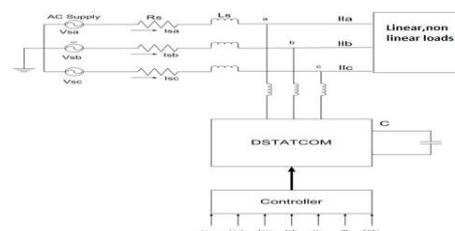


Figure 1: Block diagram of the ANN controlled DSTATCOM

IV. DSTATCOM VOLTAGE CONTROLLER

The aim of the control scheme is to maintain constant voltage magnitude at the point where a sensitive load is connected. The control system only measures the r.m.s voltage at the load point, i.e., no reactive power measurements are required. The VSC switching order is based on a sinusoidal PWM technique which offers simplicity and good response. PWM methods offer a more flexible option for a low power application which is the existing system. Thus the new approach of using the artificial neural network controlled controller for DSTATCOM is proposed in this project.

A. EXISTING SYSTEM: Sinusoidal Pulse Width Modulation control

In pulse width modulation control, the converter switches are turned on and off several times during a half cycle and the output voltage is controlled by varying the width of the pulses. The gate signals are generated by comparing a triangular wave with a DC signal. The lower order harmonics can be eliminated or reduced by selecting the number of pulses per half cycle. However increasing the number of pulses would also increase the magnitude of higher order harmonics which could easily be filtered out.

The width of the pulses can be varied to control the output voltage. However the pulse width of pulses could be different. It is possible to choose the widths of pulses in such a way that certain harmonics can be eliminated. The most common way of varying the width of the pulses is the Sinusoidal Pulse Width Modulation. In SPWM the displacement factor is unity and the power factor is improved. The lower order harmonics are eliminated and reduced. The SPWM pulses are generated and the DSTATCOM was controlled in the open loop response.

B. PROPOSED SYSTEM: Artificial Neural architecture

A BP algorithm is implemented in a three phase shunt connected custom power device known as DSTATCOM for the extraction of the weighted value of load active power and reactive power current components in nonlinear loads. The BP algorithm is used for harmonic suppression and load balancing in PFC and zero voltage regulation (ZVR) modes with dc voltage regulation of DSTATCOM. In this BP algorithm, the training of weights has three stages.

- Feed forward of the input signal training,
- Calculation and BP of the error signals,
- Upgrading of training weights.

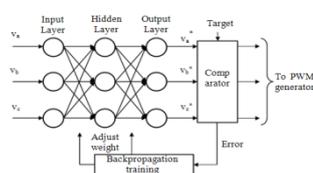


Figure 4 : Standard model of BP algorithm

The BP algorithm has one or more than one layer. It is based on a mathematical formula and does not need special features of function in the learning process. It also has smooth variation on weight correction due to batch updating features on weights. It is slow during the training process due to more number of learning steps, but after the training of weights, the algorithm produces very fast trained output response. Continuity, non-decreasing monotony and differentiability are the main characteristics of BP algorithm. In this application, the proposed control algorithm on a DSTATCOM is implemented for the compensation of nonlinear loads.

The initial output pattern is compared with the desired output pattern and the weights are adjusted by the algorithm to minimize the error. The iterative process finishes when the error becomes near null.

REFERENCE CURRENT GENERATION

A BP training algorithm is used to estimate the three phase weighted value of load active power current components (w_{ap} , w_{bp} and w_{cp}) and reactive power current components (w_{aq} , w_{bq} , and w_{cq}) from polluted load currents using the feed forward and supervised principle.

A. DERIVATION OF REFERENCE CURRENTS

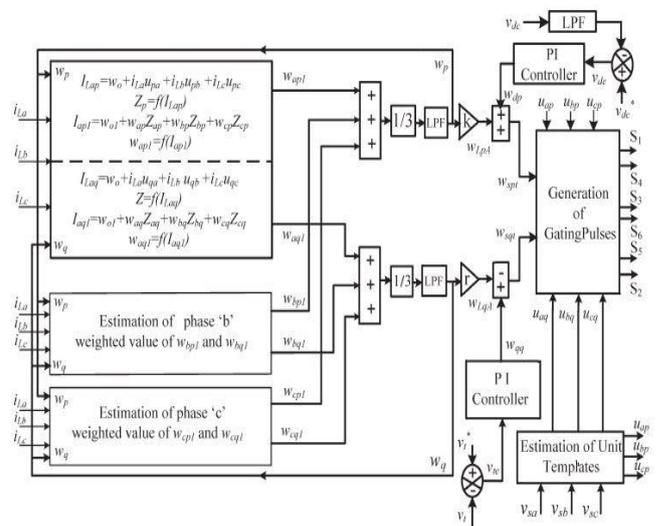


Figure 5 : Proposed modeling of BP algorithm

In this estimation, the input layer for three phases (a, b, and c) is expressed as

$$I_{Lap} = w_o + i_{La}u_{ap} + i_{Lb}u_{bp} + i_{Lc}u_{cp} \quad (1)$$

$$I_{Lbp} = w_o + i_{Lb}u_{bp} + i_{Lc}u_{cp} + i_{La}u_{ap} \quad (2)$$

$$I_{Lcp} = w_o + i_{Lc}u_{cp} + i_{La}u_{ap} + i_{Lb}u_{bp} \quad (3)$$

Where w_o is the selected value of the initial weight and u_{ap} , u_{bp} , and u_{cp} are the in-phase unit templates.

In-phase unit templates are estimated using sensed PCC phase voltages (v_{sa} , v_{sb} and v_{sc}). It is the relation of the phase voltage and the amplitude of the PCC voltage (v_t). The amplitude of sensed PCC voltages is estimated as

$$v_t = \sqrt{[2(v_{sa}^2 + v_{sb}^2 + v_{sc}^2)/3]} \quad (4)$$

The in-phase unit templates of PCC voltages (u_{ap} , u_{bp} , and u_{cp}) are estimated as [13]

$$\begin{aligned} u_{ap} &= v_{sa}/v_t & u_{bp} &= v_{sb}/v_t \\ u_{cp} &= v_{sc}/v_t \end{aligned} \quad (5)$$

The extracted values of I_{Lap} , I_{Lbp} and I_{Lcp} are passed through a sigmoid function as an activation function, and the output signals (Z_{ap} , Z_{bp} , and Z_{cp}) of the feed forward section are expressed as

$$Z_{ap} = f(I_{Lap}) = 1/(1 + e^{-I_{Lap}}) \quad (6)$$

$$Z_{bp} = f(I_{Lbp}) = 1/(1 + e^{-I_{Lbp}}) \quad (7)$$

$$Z_{cp} = f(I_{Lcp}) = 1/(1 + e^{-I_{Lcp}}) \quad (8)$$

The estimated values of Z_{ap} , Z_{bp} and Z_{cp} are fed to a hidden layer as input signals. The three phase outputs of this layer (I_{ap1} , I_{bp1} and I_{cp1}) before the activation function are expressed as

$$I_{ap1} = w_{o1} + w_{ap}Z_{ap} + w_{bp}Z_{bp} + w_{cp}Z_{cp} \quad (9)$$

$$I_{bp1} = w_{o1} + w_{bp}Z_{bp} + w_{cp}Z_{cp} + w_{ap}Z_{ap} \quad (10)$$

$$I_{cp1} = w_{o1} + w_{cp}Z_{cp} + w_{ap}Z_{ap} + w_{bp}Z_{bp} \quad (11)$$

Where w_{o1} , w_{ap} , w_{bp} , and w_{cp} are the selected value of the initial weight in the hidden layer and the updated values of three phase weights using the average weighted value (w_p) of the active power current component as a feedback signal, respectively.

The updated weight of phase “a” active power current components of load current “ w_{ap} ” at the nth sampling instant is expressed as

$$w_{ap}(n) = w_p(n) + \mu \{w_p(n) - w_{ap1}(n)\} f'(I_{ap1})Z_{ap}(n) \quad (12)$$

Where $w_p(n)$ and $w_{ap}(n)$ are the average weighted value of the active power component of load currents and the updated weighted value of phase “a” at the nth sampling instant, respectively, and $w_{ap1}(n)$ and $z_{ap}(n)$ are the phase “a” fundamental weighted amplitude of the active power

component of the load current and the output of the feed forward section of the algorithm at the nth instant, respectively. $f(I_{ap1})$ and μ are represented as the derivative of I_{ap1} components and the learning rate.

Similarly, for phase “b” and phase “c,” the updated weighted values of the active power current components of the load current are expressed as

$$w_{bp}(n) = w_p(n) + \mu \{w_p(n) - w_{bp1}(n)\} f'(I_{bp1})Z_{bp}(n) \quad (13)$$

$$w_{cp}(n) = w_p(n) + \mu \{w_p(n) - w_{cp1}(n)\} f'(I_{cp1})Z_{cp}(n) \quad (14)$$

The extracted values of I_{ap1} , I_{bp1} , and I_{cp1} are passed through a sigmoid function as an activation function to the estimation of the fundamental active components in terms of three phase weights w_{ap1} , w_{bp1} , and w_{cp1} as

$$w_{ap1} = f(I_{ap1}) = 1/(1 + e^{-I_{ap1}}) \quad (15)$$

$$w_{bp1} = f(I_{bp1}) = 1/(1 + e^{-I_{bp1}}) \quad (16)$$

$$w_{cp1} = f(I_{cp1}) = 1/(1 + e^{-I_{cp1}}) \quad (17)$$

The average weighted amplitude of the fundamental active power components (w_p) is estimated using the amplitude sum of three phase load active power components (w_{ap1} , w_{bp1} and w_{cp1}) divided by three. It is required to realize load balancing features of DSTATCOM. Mathematically, it is expressed as

$$w_p = (w_{ap1} + w_{bp1} + w_{cp1})/3 \quad (18)$$

First-order low-pass filters are used to separate the low frequency components. “k” denotes the scaled factor of the extracted active power components of current in the algorithm. After separating the low-frequency components and scaling to the actual value because the output of the activation function is between 0 and 1, it is represented as w_{Lpa} . Similarly, the weighted amplitudes of the reactive power components of the load currents (w_{aq} , w_{bq} , and w_{cq}) of the fundamental load current are extracted as

$$I_{Laq} = w_o + i_{La}u_{aq} + i_{Lb}u_{bq} + i_{Lc}u_{cq} \quad (19)$$

$$I_{Lbq} = w_o + i_{La}u_{aq} + i_{Lb}u_{bq} + i_{Lc}u_{cq} \quad (20)$$

$$I_{Lcq} = w_o + i_{La}u_{aq} + i_{Lb}u_{bq} + i_{Lc}u_{cq} \quad (21)$$

Where w_o is the selected value of the initial weight and u_{aq} , u_{bq} and u_{cq} are the quadrature components of the unit template.

The quadrature unit templates (u_{aq} , u_{bq} , and u_{cq}) of the phase PCC voltage are estimated using (5) as

$$u_{aq} = (-u_{bp} + u_{cp}) / \sqrt{3}, \quad u_{bq} = (3u_{ap} + u_{bp} - u_{cp}) / 2\sqrt{3}, \quad u_{cq} = (-3u_{ap} + u_{bp} - u_{cp}) / 2\sqrt{3} \quad (22)$$

The extracted values of I_{Laq} , I_{Lbq} , and I_{Lcq} are passed through a sigmoid function as an activation function to the estimation of Z_{aq} , Z_{bq} , and Z_{cq}

$$Z_{aq} = f(I_{Laq}) = 1 / (1 + e^{-I_{Laq}}) \quad (23)$$

$$Z_{bq} = f(I_{Lbq}) = 1 / (1 + e^{-I_{Lbq}}) \quad (24)$$

$$Z_{cq} = f(I_{Lcq}) = 1 / (1 + e^{-I_{Lcq}}) \quad (25)$$

The estimated values of Z_{aq} , Z_{bq} , and Z_{cq} are fed to the hidden layer as input signals. The three phase outputs of this layer (I_{aq1} , I_{bq1} , and I_{cq1}) before the activation function can be represented as

$$I_{aq1} = w_{o1} + w_{aq}Z_{aq} + w_{bq}Z_{bq} + w_{cq}Z_{cq} \quad (26)$$

$$I_{bq1} = w_{o1} + w_{aq}Z_{aq} + w_{bq}Z_{bq} + w_{cq}Z_{cq} \quad (27)$$

$$I_{cq1} = w_{o1} + w_{aq}Z_{aq} + w_{bq}Z_{bq} + w_{cq}Z_{cq} \quad (28)$$

Where w_{o1} , w_{aq} , w_{bq} , and w_{cq} are the selected value of the initial weight in the hidden layer and the updated three weights using the average weighted value of the reactive power components of currents (w_q) as a feedback signal, respectively.

The updated weight of the phase “a” reactive power components of load currents “ w_{aq} ” at the nth sampling instant is expressed as

$$w_{aq}(n) = w_q(n) + \mu \{w_q(n) - w_{aq1}(n)\} f'(I_{aq1})Z_{aq}(n) \quad (29)$$

$w_q(n)$ and $w_{aq}(n)$ are the average weighted value of the active power component of load currents and the updated weight in the nth sampling instant, respectively, and $w_{aq1}(n)$ and $z_{aq}(n)$ are the phase “a” weighted amplitude of the reactive power current component of load currents and the output of the feed forward section of the algorithm at the nth instant, respectively. $f'(I_{aq1})$ and μ are presented as the derivative of I_{aq1} components and the learning rate.

Similarly, for phase “b” and phase “c,” the updated weighted values of the reactive power current components of the load current are expressed as

$$w_{bq}(n) = w_q(n) + \mu \{w_q(n) - w_{bq1}(n)\} f'(I_{bq1})Z_{bq}(n) \quad (30)$$

$$w_{cq}(n) = w_q(n) + \mu \{w_q(n) - w_{cq1}(n)\} f'(I_{cq1})Z_{cq}(n) \quad (31)$$

The extracted values of I_{aq1} , I_{bq1} , and I_{cq1} are passed through an activation function to the estimation of the fundamental reactive component in terms of three phase weights w_{aq1} , w_{bq1} , and w_{cq1} as

$$w_{aq1} = f(I_{aq1}) = 1 / (1 + e^{-I_{aq1}}) \quad (32)$$

$$w_{bq1} = f(I_{bq1}) = 1 / (1 + e^{-I_{bq1}}) \quad (33)$$

$$w_{cq1} = f(I_{cq1}) = 1 / (1 + e^{-I_{cq1}}) \quad (34)$$

The average weight of the amplitudes of the fundamental reactive power current components (w_q) is estimated using the amplitude sum of the three phase load reactive power components of the load current (w_{aq1} , w_{bq1} , and w_{cq1}) divided by three. Mathematically, it is expressed as

$$w_q = (w_{aq1} + w_{bq1} + w_{cq1}) / 3 \quad (35)$$

First-order low-pass filters are used to separate the low frequency component. “r” denotes the scaled factor of the extracted reactive power components in the algorithm. After separating low-frequency components and scaling to the actual value because the output of the activation function is between 0 and 1, it is represented as w_{LqA} .

A. Amplitude of Active Power Current Components of Reference Source Currents

An error in the dc bus voltage is obtained after comparing the reference dc bus voltage v_{dc}^* and the sensed dc bus voltage v_{dc} of a VSC, and this error at the nth sampling instant is expressed as

$$v_{de}(n) = v_{dc}^*(n) - v_{dc}(n). \quad (36)$$

This voltage error is fed to a proportional–integral (PI) controller whose output is required for maintaining the dc bus voltage of the DSTATCOM. At the nth sampling instant, the output of the PI controller is as follows

$$w_{dp}(n) = w_{dp}(n-1) + k_{pd} \{v_{de}(n) - v_{de}(n-1)\} + k_{id} v_{de}(n) \quad (37)$$

Where k_{pd} and k_{id} are the proportional and integral gain constants of the dc bus PI controller. $v_{de}(n)$ and $v_{de}(n-1)$ are the dc bus voltage errors in the nth and (n-1)th instant, and $w_{dp}(n)$ and $w_{dp}(n-1)$ are the amplitudes of the active power component of the fundamental reference current at the nth and (n-1)th instant, respectively.

The amplitude of the active power current components of the reference source current (w_{spt}) is estimated by the addition of the output of the dc bus PI controller (w_{dp}) and the average magnitude of the load active currents (w_{LpA}) as

$$w_{spt} = w_{dp} + w_{LpA}. \quad (38)$$

B. Amplitude of Reactive Power Components of Reference Source Currents:

An error in the ac bus voltage is achieved after comparing the amplitudes of the reference ac bus voltage v_t^* and the sensed ac bus voltage v_t of a VSC. The extracted ac bus voltage error v_t at the nth sampling instant is expressed as

$$v_{te}(n) = v_t^*(n) - v_t(n) \quad (39)$$

The weighted output of the ac bus PI controller w_{qq} for regulating the ac bus terminal voltage at the n th sampling instant is expressed as

$$w_{qq}(n) = w_{qq}(n-1) + k_{pt} \{v_{te}(n) - v_{te}(n-1)\} + k_{it} v_{te}(n) \quad (40)$$

Where $w_{qq}(n)$ is part of the reactive power component of the source current and it is renamed as w_{qq} . K_{pt} and k_{it} are the proportional and integral gain constants of the ac bus voltage PI controller.

The amplitude of the reactive power current components of the reference source current (w_{sqt}) is calculated by subtracting the output of the voltage PI controller (w_{qq}) and the average load reactive currents (w_{LqA}) as

$$w_{sqt} = w_{qq} - w_{LqA} \quad (41)$$

C. Estimation of Reference Source Currents and Generation of IGBT Gating Pulses:

Three phase reference source active and reactive current components are estimated using the amplitude of three phase (a, b and c) load active power current components, PCC voltage in-phase unit templates, reactive power current components, and PCC quadrature voltage unit templates as

$$i_{sap} = w_{spt} u_{ap}, i_{sbp} = w_{spt} u_{bp}, i_{scp} = w_{spt} u_{cp} \quad (42)$$

$$i_{saq} = w_{sqt} u_{aq}, i_{sbq} = w_{sqt} u_{bq}, i_{scq} = w_{sqt} u_{cq} \quad (43)$$

The addition of reference active and reactive current components is known as reference source currents, and these are given as

$$I_{sa}^* = i_{sap} + i_{saq}, I_{sb}^* = i_{sbp} + i_{sbq}, I_{sc}^* = i_{scp} + i_{scq} \quad (44)$$

The sensed source currents (i_{sa}, i_{sb}, i_{sc}) and the reference source currents ($i_{sa}^*, i_{sb}^*, i_{sc}^*$) are compared, and current error signals are amplified through PI current regulators; their outputs are fed to a pulse width modulation (PWM) controller to generate the gating signals for insulated-gate bipolar transistors (IGBTs) S1 to S6 of the VSC used as a DSTATCOM

V. SIMULATION AND RESULTS

A. EXISTING SYSTEM: PWM CONTROLLED DSTATCOM

This shows the Simulink modeling of DSTATCOM in which the gate signals are generated by the PWM controller. The VSC switching strategy is based on a sinusoidal PWM technique which offers simplicity and good response. Since custom power is a relatively low-power application, PWM methods offer a more flexible option which is the existing system.

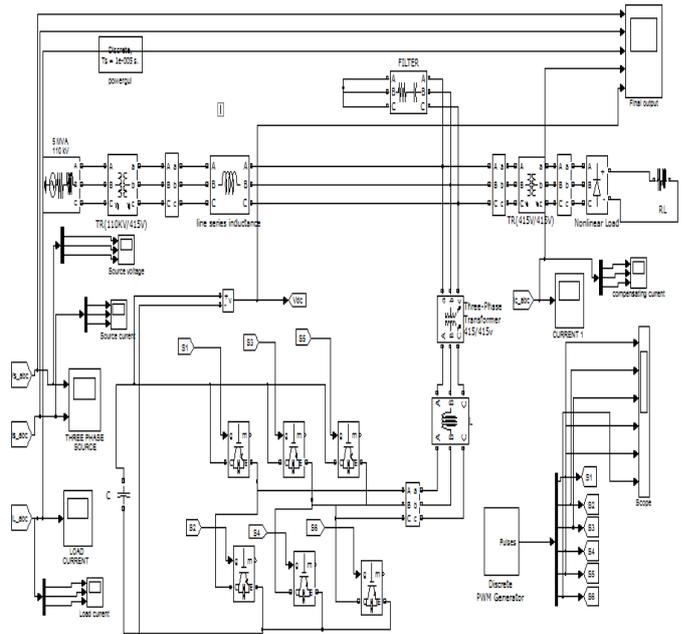


Figure 6 : Simulink modeling of PWM controlled DSTATCOM

B. RESULTS OF PWM CONTROLLED DSTATCOM

The below figure shows the waveform of source currents (i_{sa}, i_{sb}, i_{sc}), load currents (i_{La}, i_{Lb}, i_{Lc}) and compensating currents (i_{ca}, i_{cb}, i_{cc}) with PCC line voltage (v_{ab}) under unbalanced nonlinear loads.

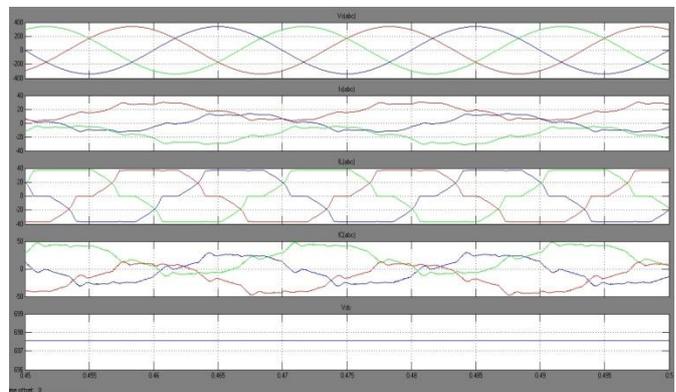


Figure 7 : Dynamic performance of DSTATCOM with PWM controller

a) V_{sabc} b) I_{sabc} c) I_{Labc} d) I_{cabc} e) V_{dc}

C. THD ANALYSIS OF PWM CONTROLLED DSTATCOM

Harmonic spectra of phase 'a' voltage at PCC (v_{sa}), source current (i_{sa}) and load current (i_{La}) are shown in figure. THDs of the phase 'a' at PCC voltage, source current, load current are observed 0.01%, 18.61% and 14.25% respectively.

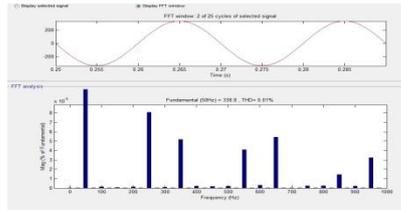


Figure 8: Waveforms and harmonic spectra of PCC voltage of phase ‘a’

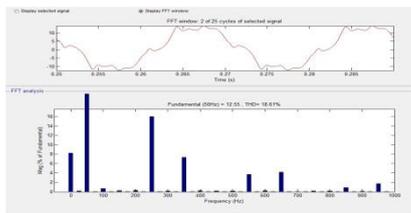


Figure 9: Waveforms and harmonic spectra of Source current of phase ‘a’

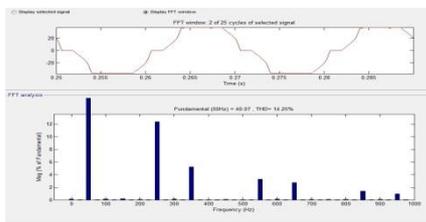


Figure 10: Waveforms and harmonic spectra of load current of phase ‘a’

D. PROPOSED SYSTEM: Neural Network Controlled DSTATCOM

The figure shows the modeling of artificial neural network controlled algorithm in the MATLAB/Simulink environment.

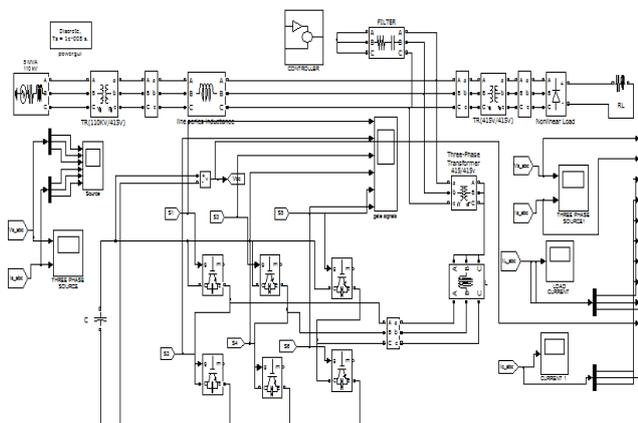


Figure 11 : Simulink Modeling of Neural Network Controlled DSTATCOM

E. UNIT TEMPLATE ESTIMATION

The figure shows the mathematical modeling of Unit template estimation which is essential for the reference current calculation in MATLAB/Simulink environment.

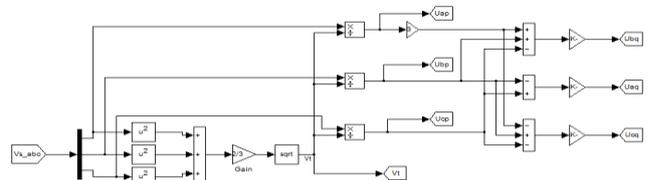


Figure 12: Mathematical modeling of Unit templates

F. REFERENCE CURRENT CALCULATION

The figure shows the mathematical modeling of reference current calculation in MATLAB/Simulink environment.

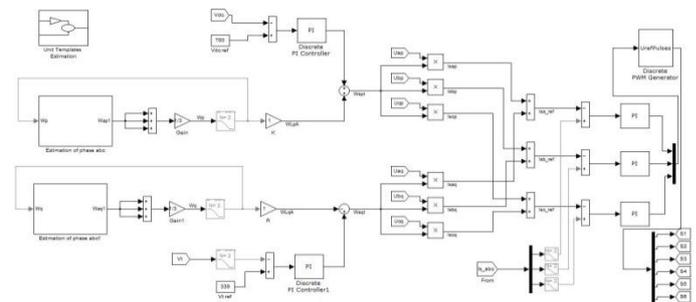


Figure 13: Mathematical modeling of Reference currents calculation

G. DSTATCOM CONTROLLER

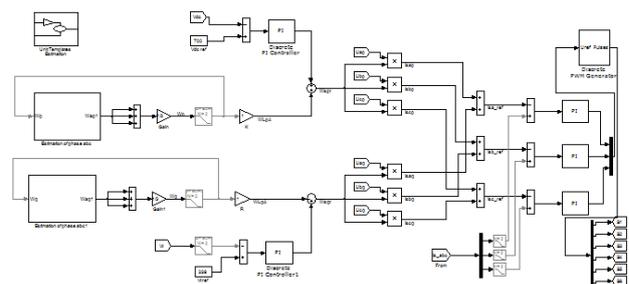


Figure 14: Mathematical Modeling of DSTATCOM controller

H. RESULTS OF NEURAL NETWORK CONTROLLED DSTATCOM

The figure shows the waveform of source currents (i_{sa} , i_{sb} , i_{sc}) load currents (i_{La} , i_{Lb} , i_{Lc}) and compensating currents (i_{Ca} , i_{Cb} , i_{Cc}) with PCC line voltage (v_{ab}) under unbalanced nonlinear loads.

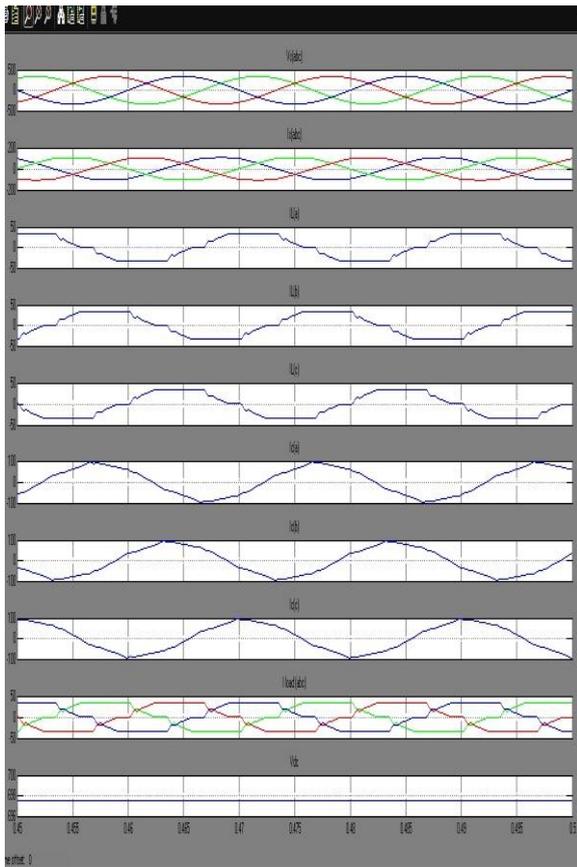


Figure 15 : Dynamic Performance of DSTATCOM under Non Linear Load in PFC mode

a) V_{Sabc} b) I_{Sabc} c) I_{La} d) I_{Lb} e) I_{Lc} f) I_{Ca} g) I_{Cb} h) I_{Cc} i) I_{Labc} j) V_{dc}

I. THD ANALYSIS OF NEURAL NETWORK CONTROLLED DSTATCOM

Harmonic spectra of phase ‘a’ voltage at PCC (v_{sa}), source current (i_{sa}) and load current (i_{La}) are shown in figure. THDs of the phase ‘a’ at PCC voltage, source current, load current are observed 0.02%, 2.46% and 11.50% respectively.

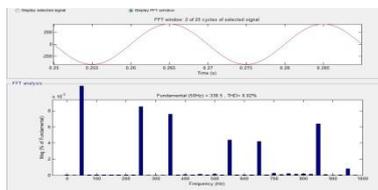


Figure 16: Waveforms and harmonic spectra of PCC voltage of phase ‘a’ in PFC mode.

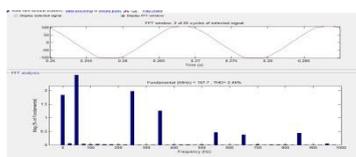


Figure 17 : Waveforms and harmonic spectra of Source current of phase ‘a’ in PFC mode

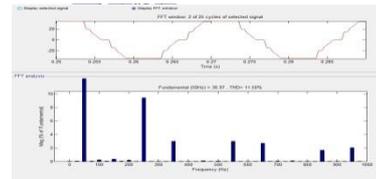


Figure 18 : Waveforms and harmonic spectra of load current of phase ‘a’ in PFC mode

VI. ANALYSIS ON THE PERFORMANCE OF DSTATCOM

| Performance parameters | DSTATCOM With PWM controller-Non Linear load (3 Phase uncontrolled rectifier with RL load) | DSTATCOM With BP controller-Non Linear load (3 Phase uncontrolled rectifier with RL load) |
|---------------------------|---|--|
| PCC voltage (V), %THD | 338.8 V,0.01% | 338.5 V,0.02% |
| Source current (A), % THD | 12.55 A,18.61% | 30.1A,2.46% |
| Load current (A),% THD | 40.06A, 14.25% | 36.97%, 11.50% |
| Dc bus voltage (V) | 700V | 700V |

Table 1: Comparative analysis on Performance of DSTATCOM in PFC mode

VII. PARAMETERS USED IN SIMULATION:

This table shows the parameters that are considered to simulate the PWM controlled DSTATCOM and the Artificial Neural Network controlled DSTATCOM.

| PARAMETERS | ANN CONTROLLED DSTATCOM | PWM CONTROLLED DSTATCOM |
|--|------------------------------------|------------------------------------|
| AC Supply Source, three phase | 415 V(L-L), 50 HZ | 415 V(L-L), 50 HZ |
| Source Impedance | $L_s = 15$ mH | $L_s = 15$ mH |
| Non-linear: Three phase full bridge uncontrolled rectifier | $R = 13\Omega$ and $L = 200$ mH | $R = 13\Omega$ and $L = 200$ mH |
| Ripple filter | $R_f = 5 \Omega$, $C_f = 10\mu F$ | $R_f = 5 \Omega$, $C_f = 10\mu F$ |
| Switching frequency of Inverter | 10kHz | 10kHz |
| Reference dc bus voltage | 700 V | 700 V |

| | | | |
|---|--------------------------|--------------------------|--|
| Interfacing Inductor(Lf) | 2.75mH | 2.75mH | [4] K.L.Sireesha , K.Bhushana Kumar “Power Quality Improvement in Distribution System Using D-STATCOM” <i>IJEAR</i> Vol. 4, Issue Spl-1, Jan - June 2014s |
| Gains of PI controller for dc bus voltage | $k_{pd}=3.1, k_{id}=0.9$ | $k_{pd}=3.1, k_{id}=0.9$ | [5] S. L. Pinjare, Arun Kumar M, “Implementation of Neural Network Back Propagation Training Algorithm on FPGA” <i>International Journal of Computer Applications</i> Volume 52– No.6, August 2012 |
| Gains of voltage PI controller | $k_{pi}=2.95, k_{it}=4$ | $k_{pi}=2.95, k_{it}=4$ | [6] Anju Tiwari, Prof. Minal Tomar “An Extensive Literature Review on Power Quality Improvement using DSTATCOM” <i>International Journal of Emerging Technology and Advanced Engineering</i> , Volume 4, Issue 5, May 2014) |
| Cut off frequency of low pass filter used in dc bus voltage | 15 Hz | 15 Hz | [7] Sujin P. Ra, T. Ruban Deva Prakashb, L. Padma Sureshc “ANN Based Voltage Flicker Mitigation with DSTATCOM Using SRF Algorithm” <i>International Journal of Current Engineering and Technology</i> , Vol.2, No.2 (June 2012) |
| Cut off frequency of low pass filter used in ac bus voltage | 10Hz | 10Hz | [8] R. C. Dugan, M. F. McGranaghan and H. W. Beaty, <i>Electric Power Systems Quality</i> , 2ed Ed., McGraw Hill, New York, 2006. |
| Cut off frequency of low pass filter used in dc bus voltage | 15 Hz | - | [9] Alfredo Ortiz, Cristina Gherasim, Mario Manana, Carlos J. Renedo, L. Ignacio Eguiluz and Ronnie J. M. Belmans, “Total harmonic distortion decomposition depending on distortion origin,” <i>IEEE Transactions on Power Delivery</i> , vol. 20, no. 4, pp. 2651-2656, October 2005. |
| Learning rate (μ) | 0.6 | - | [10] Tzung Lin Lee and Shang Hung Hu, “Discrete frequency-tuning activefilter to suppress harmonic resonances of closed-loop distribution powersystems,” <i>IEEE Transactions on Power Electronics</i> , vol. 26, no. 1, pp.137-148, January 2011. |

Table 2: Parameters of the PWM controlled DSTATCOM and ANN controlled DSTATCOM

VIII. CONCLUSION

A three phase VSC based DSTATCOM has been implemented for compensation of nonlinear loads using BPT control algorithm to verify its effectiveness. The proposed algorithm has been used for extraction of reference source currents to generate the switching pulses for IGBTs of VSC of DSTATCOM. Various functions of DSTATCOM such as, load balancing and harmonic elimination have been demonstrated in PFC mode with DC voltage regulation of DSTATCOM.

From simulation and implementation results, it is concluded that DSTATCOM and its control algorithm have been found suitable for compensation of nonlinear loads. These results show satisfactory performance of the BP control algorithm for harmonics elimination according to IEEE-519 guidelines in order of less than 5%. The DC bus voltage of the DSTATCOM has also been regulated to rated value without any overshoot or undershoots during load variation. Large training time in the application of complex system, selection of number of hidden layer in system is the disadvantage of this algorithm.

REFERENCES

[1] Bhim Singh, P. Jayaprakash, D. P. Kothari, Ambrish Chandra, Kamal Al Haddad “Comprehensive Study of DSTATCOM Configurations” *IEEE Transactions on Industrial Informatics*, VOL. 10, NO. 2, MAY 2014

[2] Bhim Singh, Sabha Raj Arya “Design and control of a DSTATCOM for power quality improvement using cross correlation function approach” *International Journal of Engineering, Science and Technology* Vol. 4, No. 1, 2012, pp. 74-86, April 2012

[3] Alpesh Mahyavanshi, M. A. Mulla, R. Chudamani “Reactive Power Compensation by Controlling the DSTATCOM” *International Journal of Emerging Technology and Advanced Engineering*, Volume 2, Issue 11, November 2012

[4] K.L.Sireesha , K.Bhushana Kumar “Power Quality Improvement in Distribution System Using D-STATCOM” *IJEAR* Vol. 4, Issue Spl-1, Jan - June 2014s

[5] S. L. Pinjare, Arun Kumar M, “Implementation of Neural Network Back Propagation Training Algorithm on FPGA” *International Journal of Computer Applications* Volume 52– No.6, August 2012

[6] Anju Tiwari, Prof. Minal Tomar “An Extensive Literature Review on Power Quality Improvement using DSTATCOM” *International Journal of Emerging Technology and Advanced Engineering*, Volume 4, Issue 5, May 2014)

[7] Sujin P. Ra, T. Ruban Deva Prakashb, L. Padma Sureshc “ANN Based Voltage Flicker Mitigation with DSTATCOM Using SRF Algorithm” *International Journal of Current Engineering and Technology*, Vol.2, No.2 (June 2012)

[8] R. C. Dugan, M. F. McGranaghan and H. W. Beaty, *Electric Power Systems Quality*, 2ed Ed., McGraw Hill, New York, 2006.

[9] Alfredo Ortiz, Cristina Gherasim, Mario Manana, Carlos J. Renedo, L. Ignacio Eguiluz and Ronnie J. M. Belmans, “Total harmonic distortion decomposition depending on distortion origin,” *IEEE Transactions on Power Delivery*, vol. 20, no. 4, pp. 2651-2656, October 2005.

[10] Tzung Lin Lee and Shang Hung Hu, “Discrete frequency-tuning activefilter to suppress harmonic resonances of closed-loop distribution powersystems,” *IEEE Transactions on Power Electronics*, vol. 26, no. 1, pp.137-148, January 2011.

[11] K. R. Padiyar, *FACTS Controllers in Power Transmission and Distribution*, New Age International, New Delhi, 2008.

[12] *IEEE Recommended Practices and requirement for Harmonic Control on electric power System*, IEEE Std.519, 1992.

[13] Tzung-Lin Lee, Shang-Hung Hu and Yu-Hung Chan, “DSTATCOM with positive-sequence admittance and negative-sequence conductance to mitigate voltage fluctuations in high-level penetration of distributed generation systems,” *IEEE Transactions on Industrial Electronics*, vol.60, no. 4, pp. 1417-1428, April 2013.

[14] B. Singh, P. Jayaprakash and D.P. Kothari, “ Power factor correction and power quality improvement in the distribution system,” *Journal of Electrical India*, pp. 40-48, April, 2008.

[15] Jinn-Chang Wu, Hung Liahng Jou, Ya Tsung Feng, Wen Pin Hsu, Min Sheng Huang, and WenJet Hou, “Novel circuit topology for three-phase active power filter,” *IEEE Transactions on Power Delivery*, vol. 22, no. 1, pp. 444-449, January 2007.

BIOGRAPHY



S. Sherin Jasper did her Bachelor of Engineering in Electrical & Electronics Engineering at Government college of Engineering, Tirunelveli and doing M.E degree in Electrical engineering with specialization in Power Electronics & Drives at Sri Shakthi Institute of Engineering and Technology, Coimbatore, India. Her research interests include Power Electronics, Power Quality.